



Robotics: Inverse Kinematics

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Kinematics tasks

- ▶ Forward kinematics (FK)
 - ▶ how to compute end-effector pose from the configuration
 - ▶ $x = f_{fk}(q)$
 - ▶ x is expressed in task-space, *i.e.* $SE(2)$, $SE(3)$, or $\mathbb{R}^2$, $\mathbb{R}^3$ for position only
 - ▶ $q \in \mathbb{R}^N$ is configuration (joint space)



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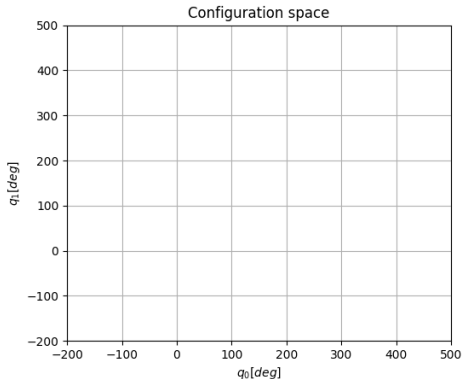
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- ▶ Differential kinematics
 - ▶ relates end-effector velocity to joint velocities
 - ▶ $\dot{\mathbf{x}} = J(\mathbf{q})\dot{\mathbf{q}}$
- ▶ Inverse kinematics (IK)
 - ▶ how to compute robot configuration(s) for given end-effector configuration
 - ▶ $\mathbf{q} \in f_{\text{ik}}(\mathbf{x})$



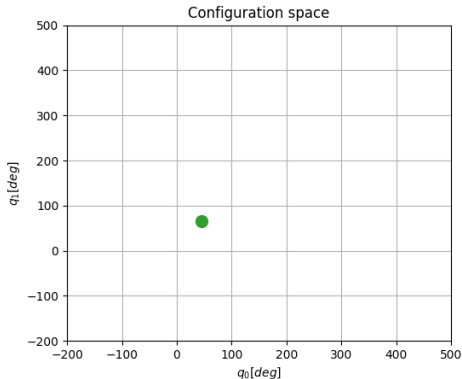
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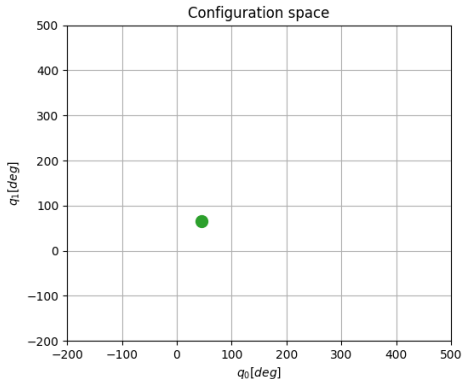
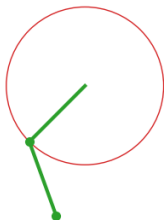
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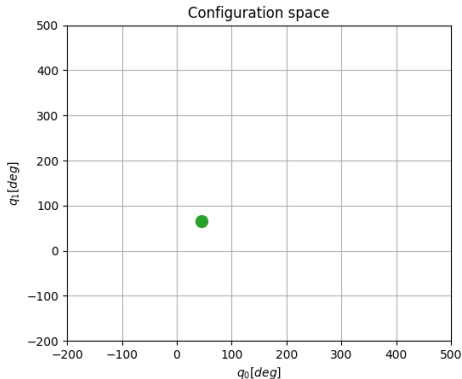
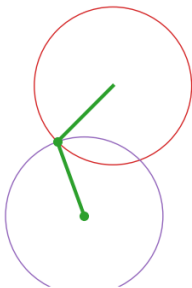
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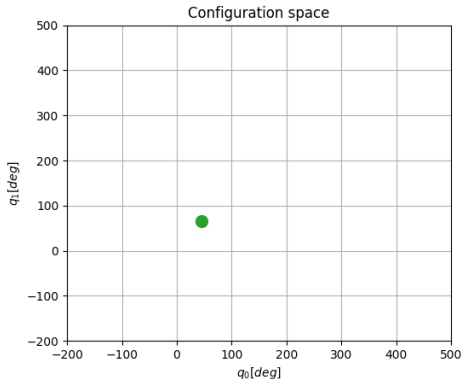
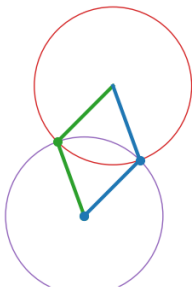
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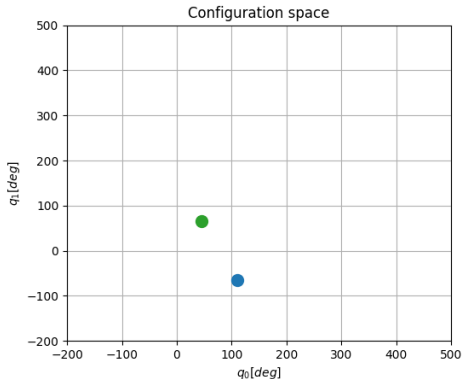
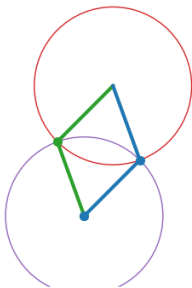
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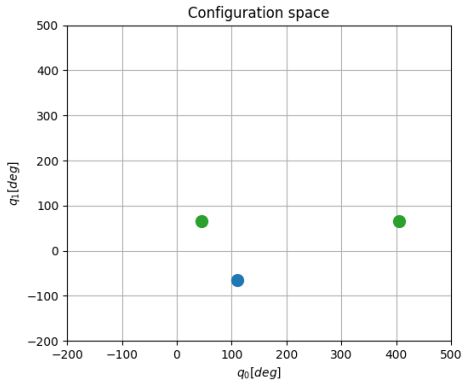
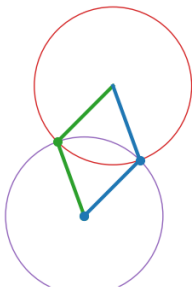
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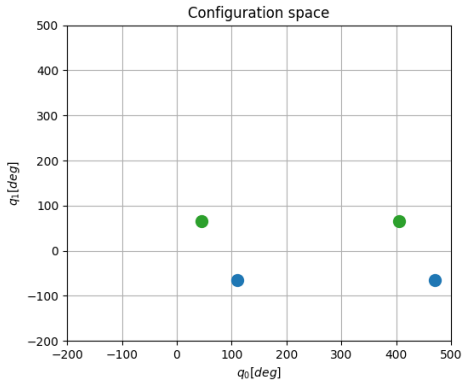
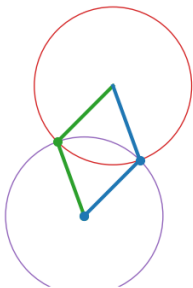
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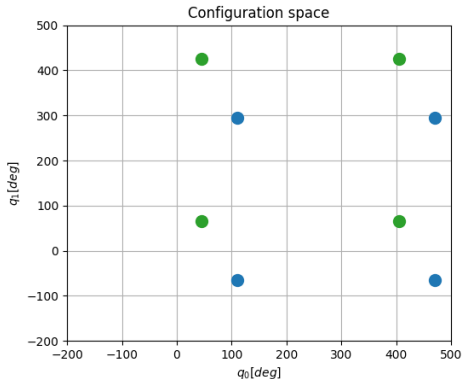
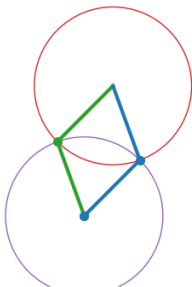
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- ▶ Task space: translation of end-effector, $\mathbf{x} \in \mathbb{R}^2$
- ▶ Configuration (joint) space: $\mathbf{q} \in \mathbb{R}^2$
- ▶ Algorithm:
 - ▶ Compute position of all joints and end-effector
 - ▶ No solution, 1 solution, 2 solutions, or ∞ solutions
 - ▶ For each solution, compute joint configurations $\theta_i = \text{atan2}(y, x) + 2k\pi, k \in \mathbb{Z}$
 $\begin{pmatrix} x & y \end{pmatrix}^\top = \mathbf{t}_{i,i+1}$, i.e. translation part of $T_{i,i+1}$



Numerical optimization

- ▶ Analytical solution is often unavailable
 - ▶ solution does not exist and we seek for the closest approximate
 - ▶ infinite solutions exist and we seek for configuration w.r.t. given criteria



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 - ▶ taylor expansion of $g(\theta)$ at θ^0 :
$$g(\theta) = g(\theta^0) + \frac{\partial g}{\partial \theta}(\theta^0)(\theta - \theta^0) + \text{higher-order terms}$$



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$$\theta \approx \theta^0 - \left(\frac{\partial g}{\partial \theta}(\theta^0) \right)^{-1} g(\theta^0)$$



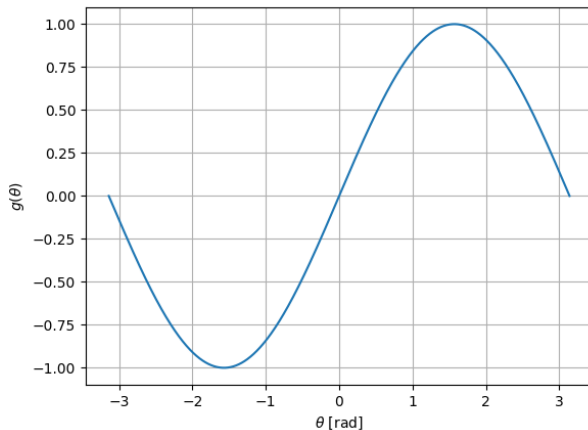
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 - ▶ as we ignore higher-order terms, we need to iterate:
$$\theta^{k+1} = \theta^k - \left(\frac{\partial g}{\partial \theta}(\theta^k) \right)^{-1} g(\theta^k)$$



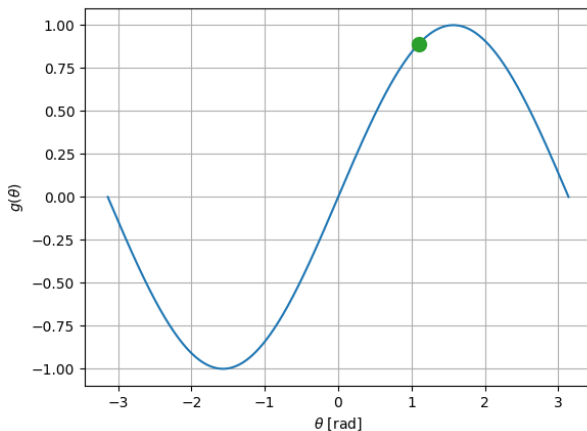
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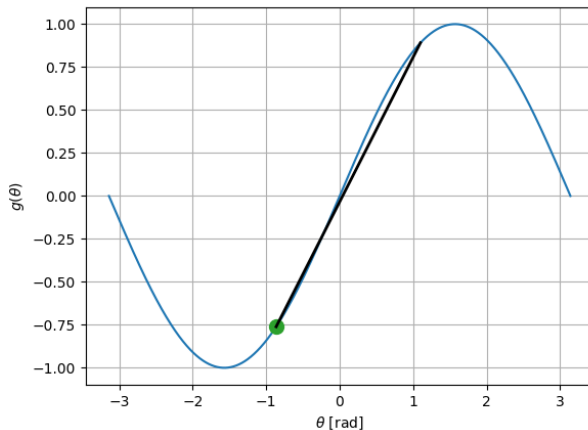
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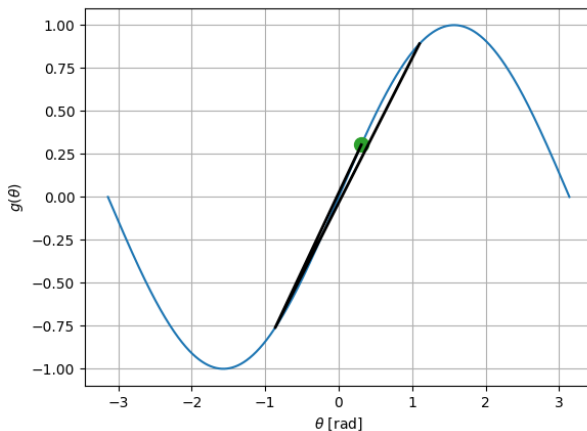
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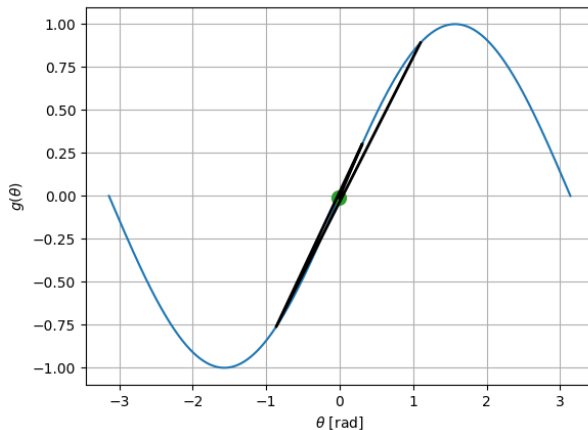
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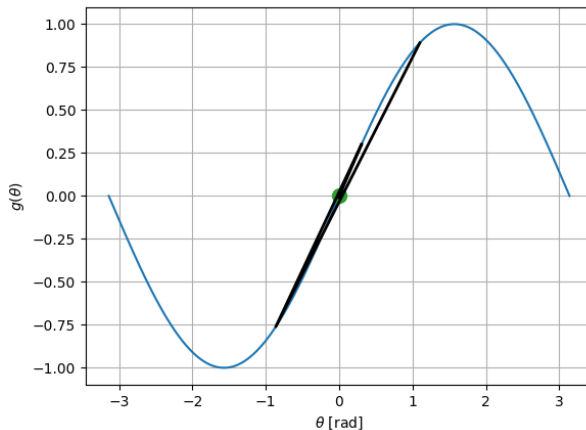
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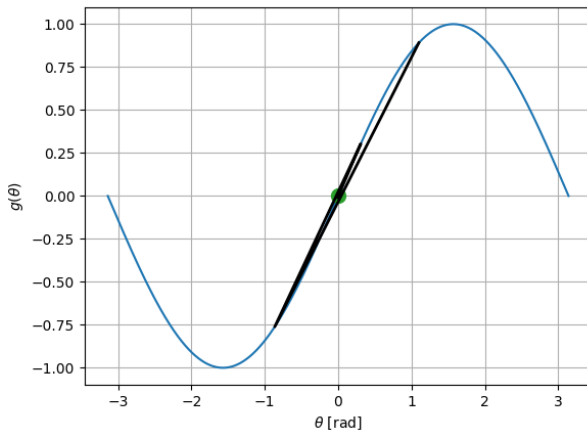
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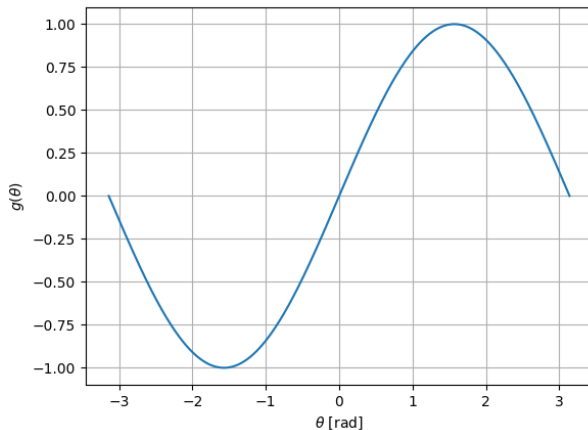
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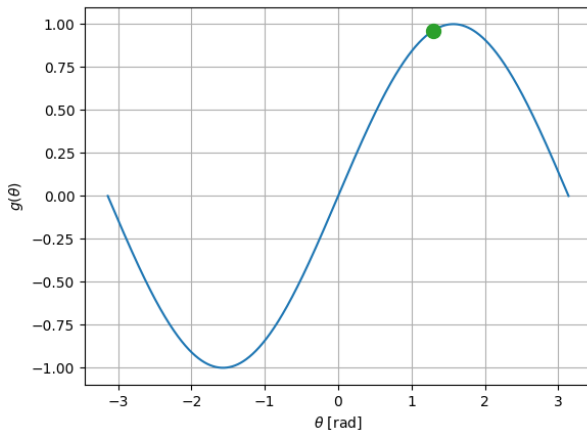
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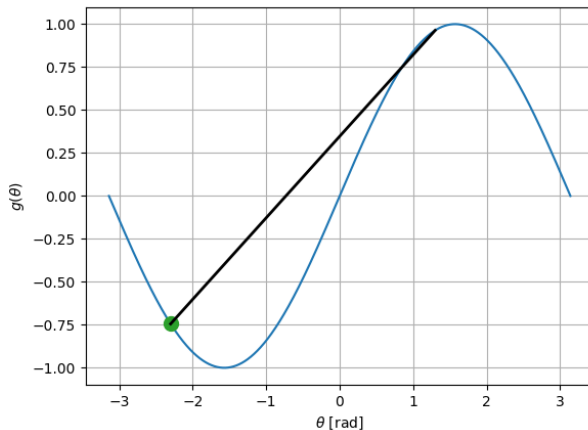
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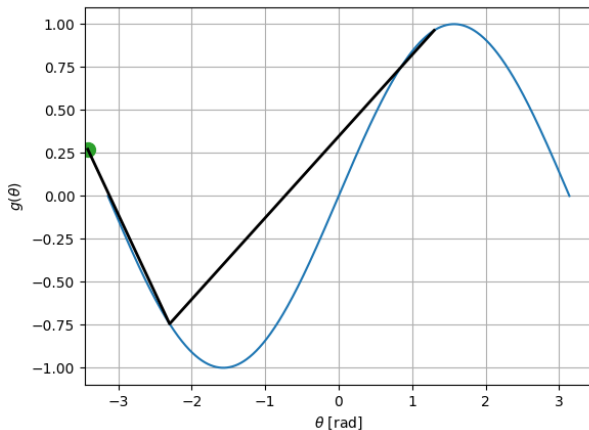
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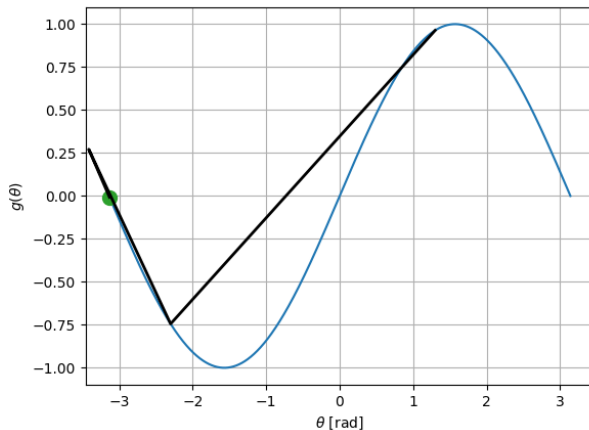
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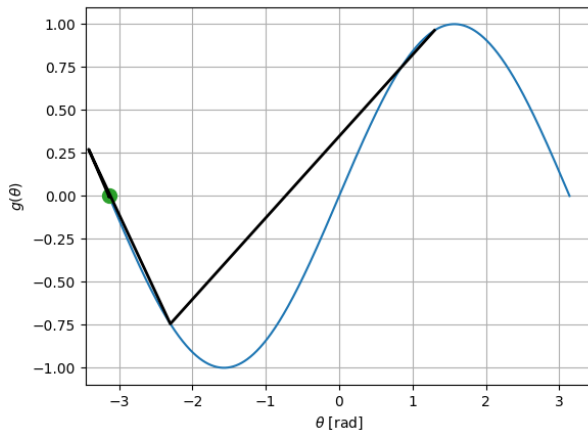
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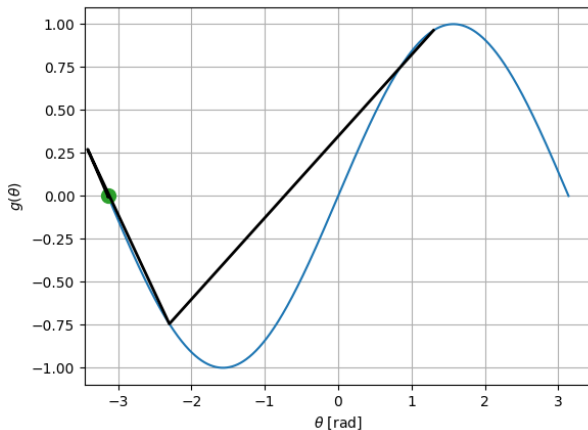
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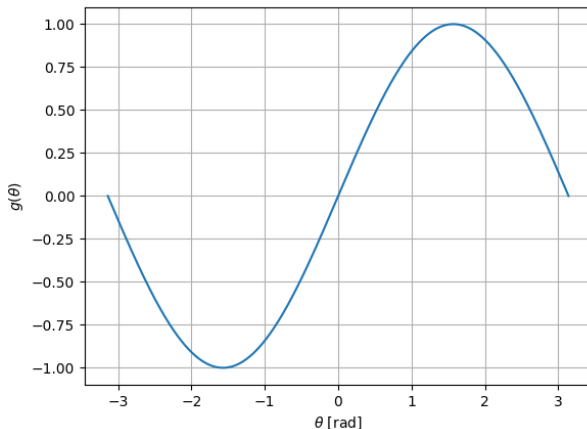
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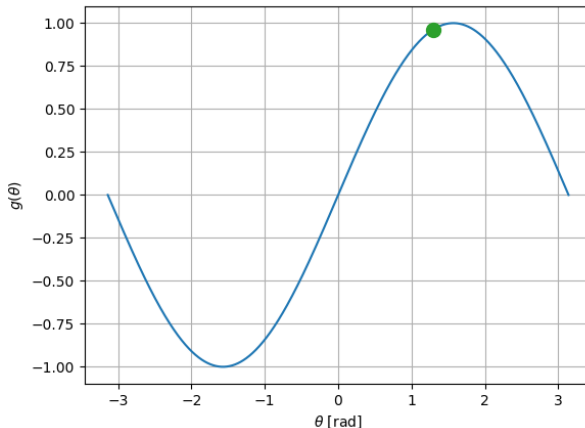
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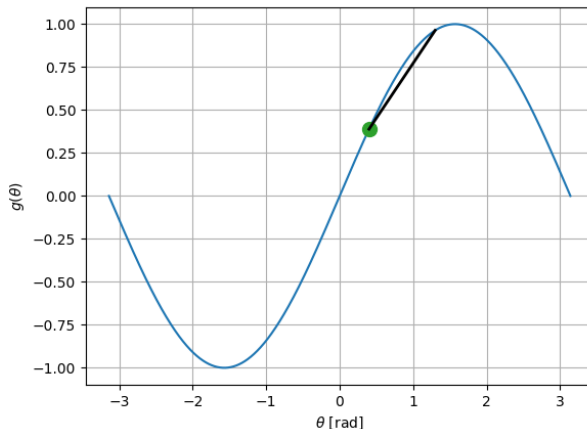
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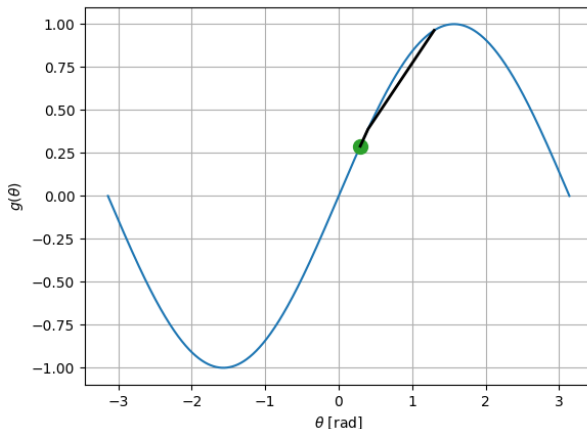
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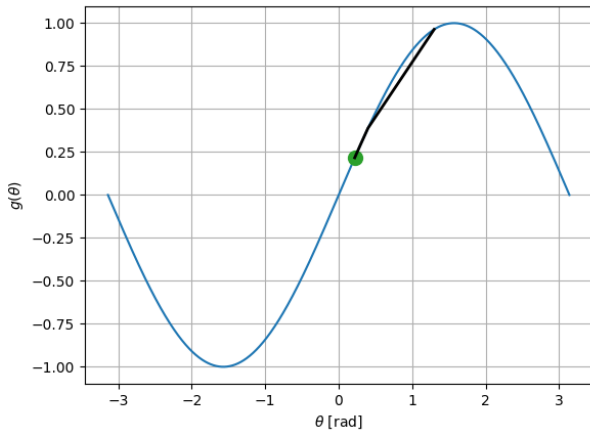
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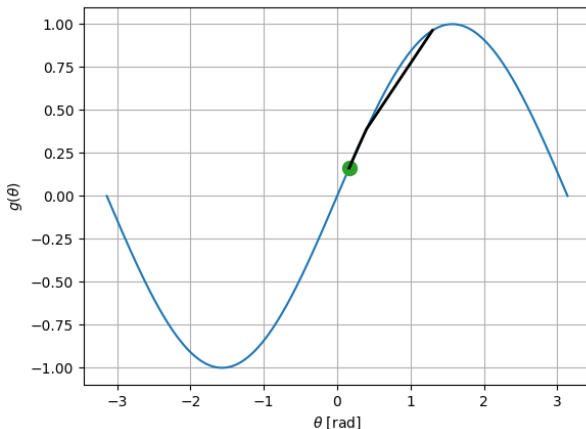
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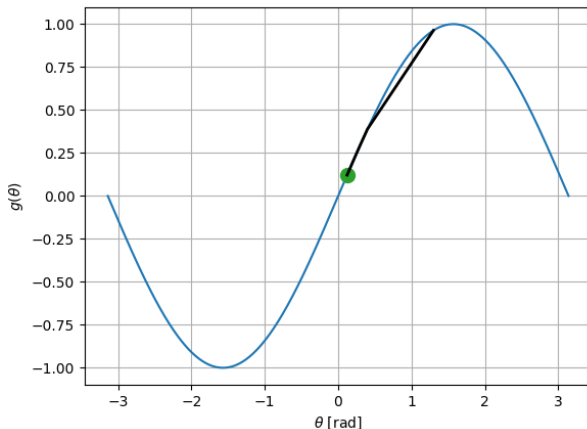
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 - ▶ repeat
- ▶ More sophisticated line-search algorithms exist



Numerical solution for RR IK

- ▶ Newton–Raphson method for n -dimensional case

$$\boldsymbol{\theta}^{k+1} = \boldsymbol{\theta}^k - \alpha \left(\frac{\partial g}{\partial \boldsymbol{\theta}}(\boldsymbol{\theta}^k) \right)^{-1} g(\boldsymbol{\theta}^k) \text{ solves } g(\boldsymbol{\theta}) = \mathbf{0}$$



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- ▶ For manipulator kinematics:
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$$\boldsymbol{\theta}^{k+1} = \boldsymbol{\theta}^k - \alpha \left(\frac{\partial g}{\partial \boldsymbol{\theta}}(\boldsymbol{\theta}^k) \right)^{-1} g(\boldsymbol{\theta}^k) \text{ solves } g(\boldsymbol{\theta}) = \mathbf{0}$$

- ▶ For manipulator kinematics:

$$g(\mathbf{q}) = \mathbf{x}_d - f_{\text{fk}}(\mathbf{q}), \mathbf{x}_d \in \mathbb{R}^2$$

- ▶ Following NR method (for $g(\mathbf{q}) = 0$):

$$\begin{aligned} \mathbf{x}_d = f_{\text{fk}}(\mathbf{q}_d) &\approx f_{\text{fk}}(\mathbf{q}^0) + \frac{\partial f_{\text{fk}}}{\partial \mathbf{q}}(\mathbf{q}^0)(\mathbf{q}_d - \mathbf{q}^0) = f_{\text{fk}}(\mathbf{q}^0) + J(\mathbf{q}^0)(\mathbf{q}_d - \mathbf{q}^0) \\ \mathbf{q}_d &\approx \mathbf{q}^0 + J(\mathbf{q}^0)^{-1}(\mathbf{x}_d - f_{\text{fk}}(\mathbf{q}^0)) \end{aligned}$$



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- ▶ Iteratively with line-search:

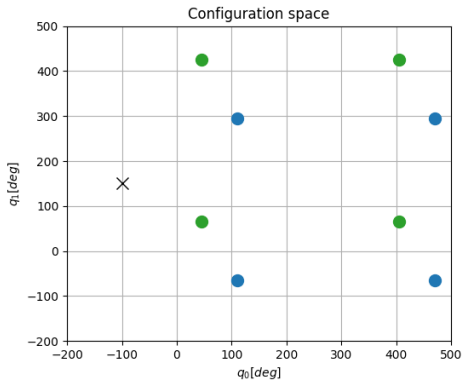
$$\mathbf{q}^{k+1} = \mathbf{q}^k + \alpha J(\mathbf{q}^k)^{-1}(\mathbf{x}_d - f_{\text{fk}}(\mathbf{q}^k))$$

- ▶ Intuition via differential kinematics:

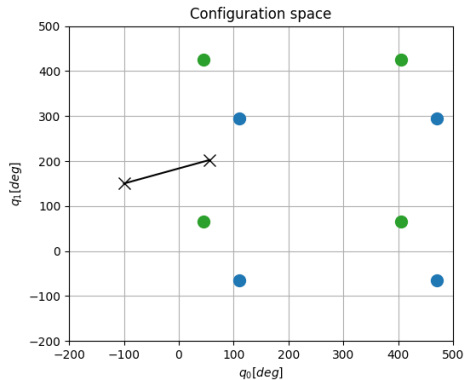
- ▶ what should be velocity in joint space s.t. we achieve given velocity in task-space
- ▶ $\dot{\mathbf{q}} = J^{-1}\dot{\mathbf{x}}$



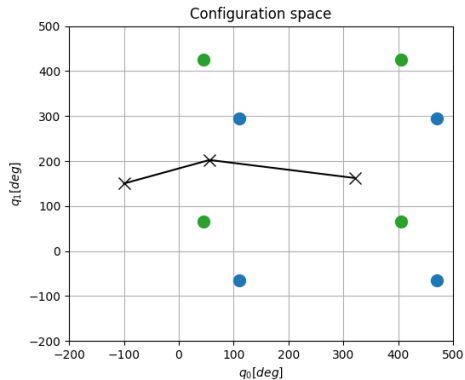
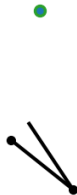
Numerical solution for RR IK #1



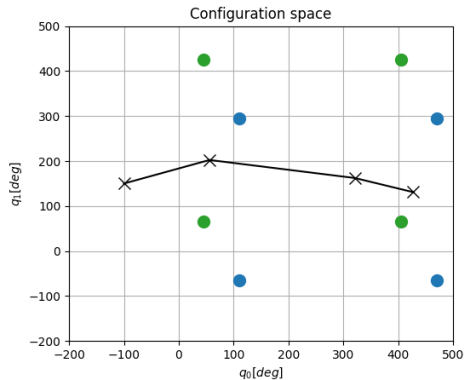
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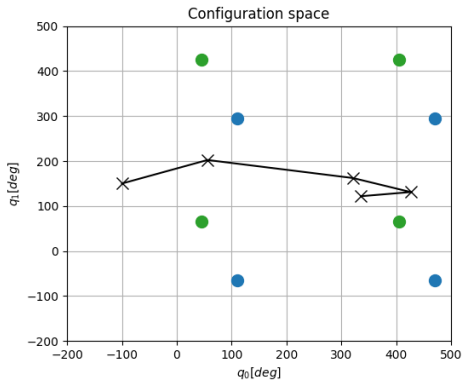
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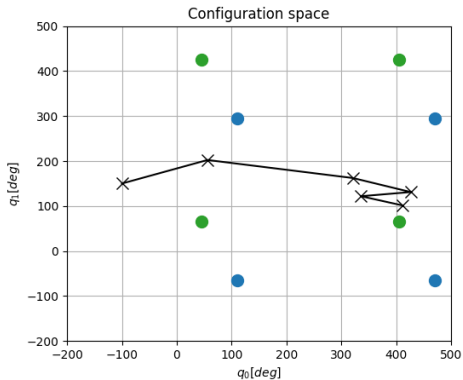
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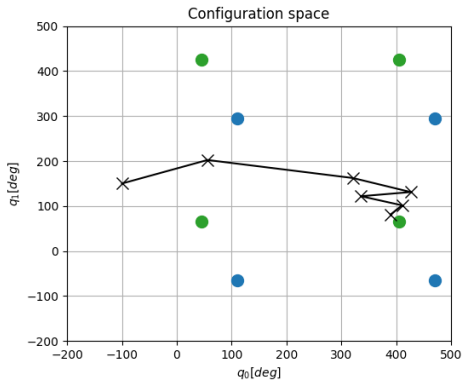
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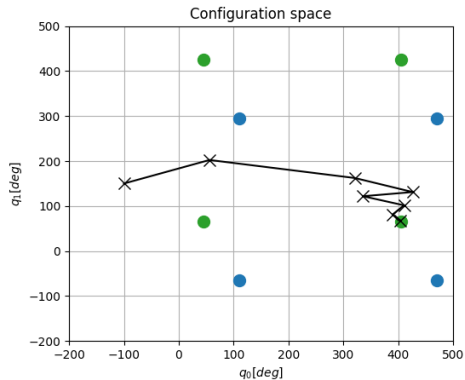
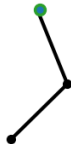
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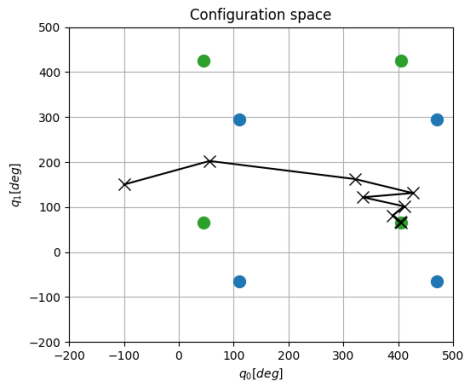
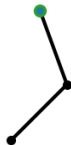
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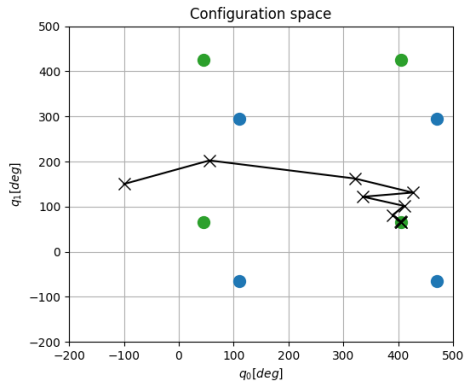
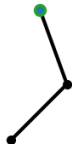
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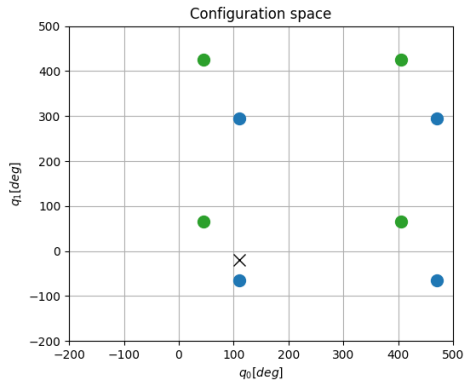
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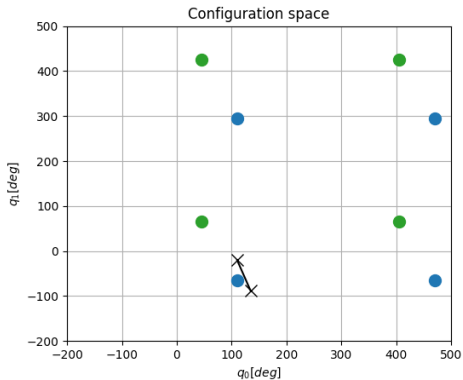
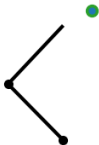
Numerical solution for RR IK #1



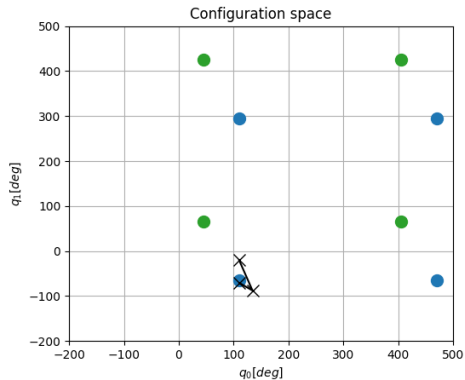
Numerical solution for RR IK #2



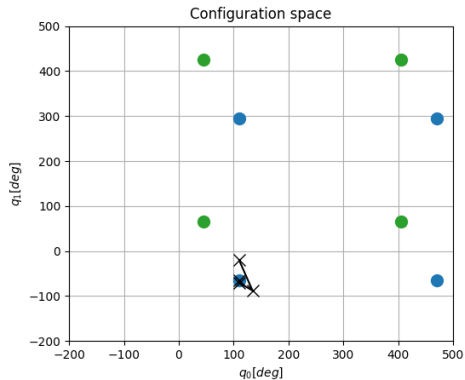
Numerical solution for RR IK #2



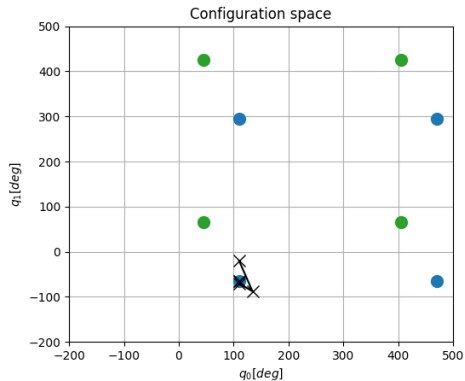
Numerical solution for RR IK #2



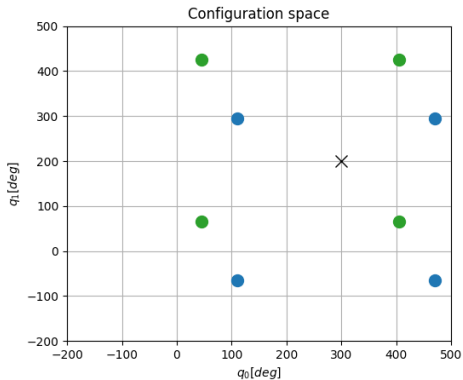
Numerical solution for RR IK #2



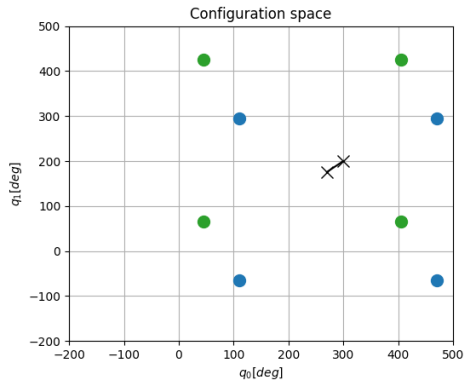
Numerical solution for RR IK #2



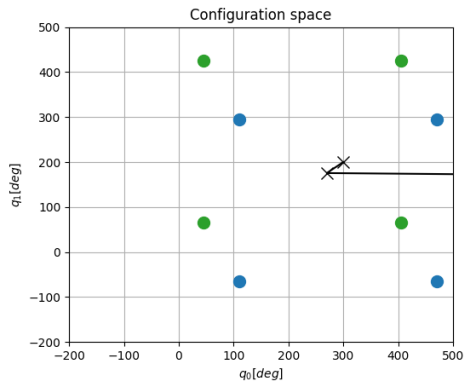
Numerical solution for RR IK #3



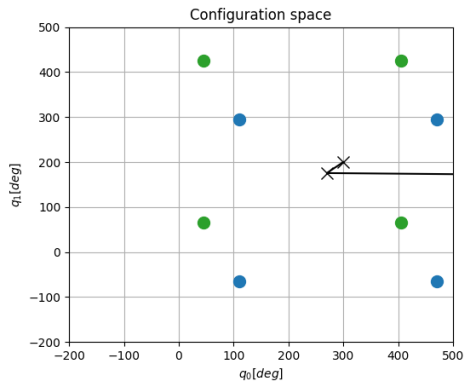
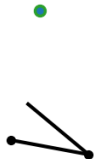
Numerical solution for RR IK #3



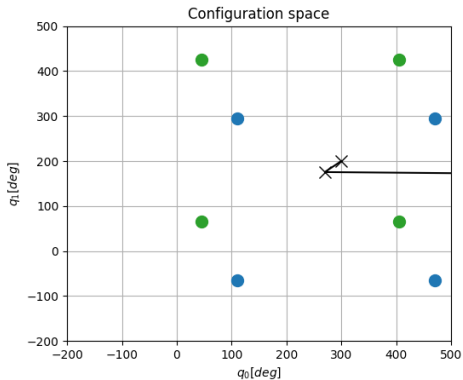
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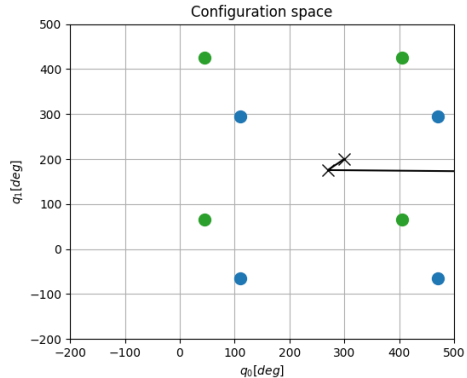
Numerical solution for RR IK #3



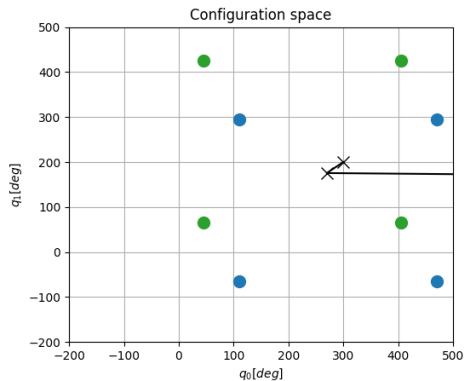
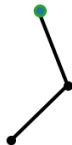
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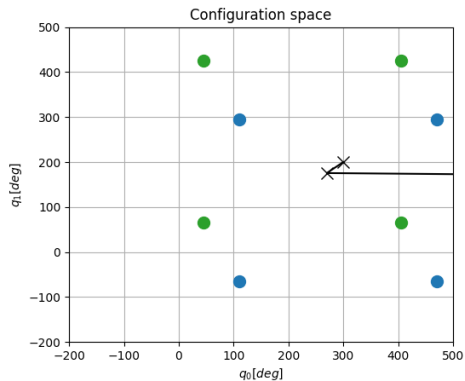
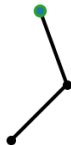
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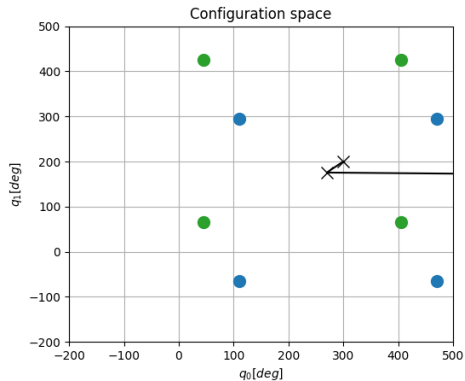
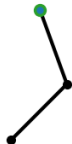
Numerical solution for RR IK #3



Numerical solution for RR IK #3



Numerical solution for RR IK #3



Numerical solution - takout message

- ▶ Numerical solution is easy to implement for general manipulators
- ▶ Initial guess is important
 - ▶ if we are *close* to the solution, FK is almost linear we will converge to the *closest* solution
 - ▶ if we are *too far away* we have no control about which solution is selected
 - ▶ tuning step-size might help
- ▶ We need to define stopping criteria
 - ▶ e.g. $\|x_d - f_{fk}(q^k)\| < \varepsilon$



What if J is not invertible?

- ▶ Redundant robots, Underactuated robots, Singularity



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- ▶ Moore–Penrose pseudoinverse $J^\dagger$
- ▶ $\mathbf{q}^{k+1} = \mathbf{q}^k + \alpha J^\dagger(\mathbf{q}^k)(\mathbf{x}_d - f_{fk}(\mathbf{q}^k))$



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 - ▶ infinite solutions to achieve same task space velocity
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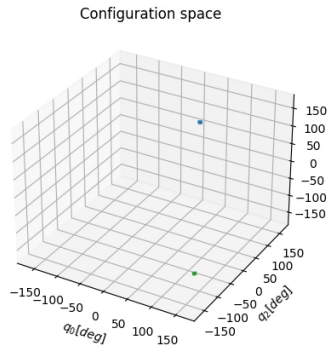


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- ▶ Redundant robots
 - ▶ infinite solutions to achieve same task space velocity
 - ▶ pseudoinverse will additionally minimize $\|\mathbf{q}\|$
- ▶ Underactuated robots or singularity
 - ▶ no exact solution exist for task space velocity
 - ▶ pseudoinverse will minimize the error in task-space



IK solution for redundant robot



IK in $SE(2)$ for RRR

- ▶ Given desired pose $T_{RG}^D \in SE(2)$
 - ▶ R - reference frame
 - ▶ G - gripper frame



IK in $SE(2)$ for RRR

- ▶ Given desired pose $T_{RG}^D \in SE(2)$
 - ▶ R - reference frame
 - ▶ G - gripper frame
- ▶ Analytical solution
 - ▶ decouple problem into rotation (last joint) and position (other joints)
 - ▶ $t_{RC} = T_{RG}^D \begin{pmatrix} -l_3 & 0 & 1 \end{pmatrix}^\top$
 - ▶ t_{RB} compute as for RR for translation task-space
 - ▶ use atan2 to compute joint configurations



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- ▶ Numerical solution
 - ▶ error in reference frame:
$$e(\mathbf{q}) = \begin{pmatrix} x_{RG}^D - x_{RG}(\mathbf{q}) & y_{RG}^D - y_{RG}(\mathbf{q}) & \phi_{RG}^D - \phi_{RG}(\mathbf{q}) \end{pmatrix}^\top$$



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- ▶ Numerical solution
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$$e(\mathbf{q}) = (x_{RG}^D - x_{RG}(\mathbf{q}) \quad y_{RG}^D - y_{RG}(\mathbf{q}) \quad \phi_{RG}^D - \phi_{RG}(\mathbf{q}))^\top$$
 - ▶ NR step:
$$\mathbf{q}^{k+1} = \mathbf{q}^k + \alpha J^\dagger(\mathbf{q}^k) e(\mathbf{q}^k)$$

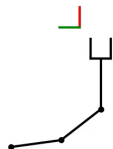


IK in $SE(2)$ for RRR

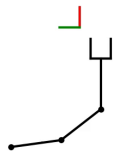
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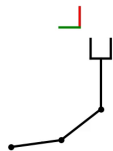
Numerical solution in $SE(2)$



Numerical solution in $SE(2)$



Numerical solution in $SE(2)$



IK in $SE(3)$

- ▶ Numerical IK algorithm is almost the same
 - ▶ error needs to be computed via transformations
 - ▶ as in planar case, error needs to be represented in reference frame



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IK in $SE(3)$

- ▶ Numerical IK algorithm is almost the same
 - ▶ error needs to be computed via transformations
 - ▶ as in planar case, error needs to be represented in reference frame
- ▶ Analytical solution might not exist for general 6 DoF manipulator
- ▶ For 6 DoF spatial robot with revolute joints
 - ▶ solution can be decoupled if last three joint axes intersect each other
 - ▶ use last three joints to orient gripper
 - ▶ use the first three joints to position the flange



Example of importance of multiple solutions



Summary

- ▶ Inverse kinematics
 - ▶ analytical solution via geometrical analysis
 - ▶ leads to computation of intersections of geometrical primitives
 - ▶ numerical solution, Newton–Raphson method
 - ▶ Jacobian
 - ▶ pseudoinverse
- ▶ Number of solutions of inverse kinematics
 - ▶ no solution
 - ▶ multiple solutions
 - ▶ periodical solutions
 - ▶ infinite number of solutions



Laboratory

- ▶ Numerical IK in $SE(2)$
- ▶ Analytical IK in $SE(2)$ for RRR manipulator
- ▶ Analytical IK in $SE(2)$ for PRR manipulator [optional]

